

REPORT OF UNDERWAY  $p\text{CO}_2$  MEASUREMENTS IN SURFACE WATERS  
AND THE ATMOSPHERE DURING November - December 2003

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**1. General**

**1-a) The Cruise:**

This cruise was to service Palmer Station and conduct biological and oceanographic research in the vicinity of the Antarctic Peninsula. The ship departed Punta Arenas, Chile on 23 November 2003, arrived at Palmer Station on 30 November. The ship departed from Palmer Station on 2 December, and arrived in Punta Arenas on 29 December 2003. Generally our system performed well. there were some periods where the flow appeared to be interrupted, and the Licor IR Analyzer appeared to be turned off for the first 2+ days. The air data continues to be highly problematic. It is highly variable, and the low mean value is near 374, higher than the Globalview  $\text{CO}_2$  value.

**1-b) The  $p\text{CO}_2$  data:**

The primary source of data are files created by the ships data acquisition system, (RVDAS). A program runs to combined  $p\text{CO}_2$  data, thermosalinograph (TSG) data, and several other parameters, such as latitude, longitude, windspeed, ship heading and speed, etc. We used raw  $p\text{CO}_2$ , TSG temperature and salinity, and position from the ship's GPS data in the merged RVDAS file. These files have the name: LMGpco2m.dxxx, where xxx is the 3 digit Julian Date.

The system performed very well, and the only editing require was to remove two periods when the water flow appeared to be interrupted.. The thermosalinograph temperature data continues to have anomalous spikes. The graph of equilibration chamber temperature versus thermosalinograph temperature shows several groups of data with slopes dramatically different from 1.0. These are eliminated, and a curve fit through the remaining data. This curve is used to estimated Sea Surface Temperature, and it is the temperature at which the  $p\text{CO}_2$  at SST is calculated.

Thirty seawater and five air observations are made between standard sets. Each observation involves flowing the equilibration gas for 120 seconds. We also flow the air for 120 seconds before stopping for an observation. Details on these and other aspects of the analysis system are explained later.

**Standards:**

Cylinder	Concentration (ppm)
Nitrogen (UHP)	0.0
CC46457	150.19
CA02237	364.44
CC22986	252.0
CC46471	788.0
CC104439	384.075

A 4<sup>th</sup> order calibration curve is used with 5 standards, not including the Nitrogen, as described in Section 2.

Standards flow for about 120 seconds before an observation is made.

**1-c) AIR data:**

There are **2,060 air observations**. By applying a mean and standard deviation filter to the data, **1,428** were retained. These gave a mean of **372.04 ± 0.48 (N = 1428)**. This compares with a value from the GlobalView CO<sub>2</sub> database extrapolated from 2002 of 373.0. Our value contains a great deal of noise, but is just within 1 ppm of the GlobalView value.

To calculate  $\Delta p\text{CO}_2$  we use the Global View CO<sub>2</sub> data, extrapolated from the end of 2001 through 2002. The last observations in that file are for year 2001. A longterm trend is fitted to these observations, then extrapolated forward. Naturally, there is some uncertainty in this extrapolation, but it should be less than ±0.5 ppm. This value goes into the "vco2\_air" and "gvvco2\_air" variables in the **L039sfc** database.

**1-d) Editing:**

The group of individual days were concatenated together and edited under the name **rawdata.txt**. Periods where the system was interrupted before a standard run was complete, those where the data are unreadable, etc. are edited at this level.

a. The TSG temperature was not reliable for most of this cruise. We use an equation derived by matlab to estimate SST. The equation uses the data where equilibration temperature is > 0.5 degrees, and the difference between equilibration temperature and TSG temperature is < 0.1°C. The result is:

$$\text{SST} = 1.0036 * \text{Equilibration Temperature} - 0.0639$$

b. Of the **12,373 observations** of seawater pCO<sub>2</sub>, we **rejected 85, retaining 12,288 records**. The program **editpco2.prg** performs this editing operation.

c. There were two periods where the temperature ramped up monotonically, while the  $v\text{CO}_2$  was essentially unchanging. We interpret this to be water flow interruption, and the data were eliminated.

d. To create a **L039sfc.dbf** surface format file, we use only ACCEPTED  $\text{pCO}_2$  values, but ALL the data are retained in the **pco2data.dbf** database in the subdirectory: \LMGOULD\2003\img03\_9\SURFACE\PCO2DATA. We estimate the air value from the Globalview CO2database (as explained under 1-d) AIR data . The program **makeL039.prg** performs this process. The program also adds salinity from the edited salinity file **saldata.dbf** in the salinity subdirectory (see other data below).

#### **1-f) Other Data:**

Salinity: There is a program, **procsal.prg** in the subdirectory salinity which performs editing of the salinity data. The system uses a mean and standard deviation of 15 data points. There are five passes through the data. Three calculate mean and standard deviation, two perform edits. After each of the first 2 calculation passes, data points are rejected if outside 1 standard deviation. A minimum standard deviation of 0.02 is assigned. After the second editing pass (4th through the data), mean and standard deviation of the remaining data are calculated using only accepted values. Between accepted values the mean is unchanged. This file **saldata.dbf** is then used as the source for salinity in the master file **L039sfc.dbf**.

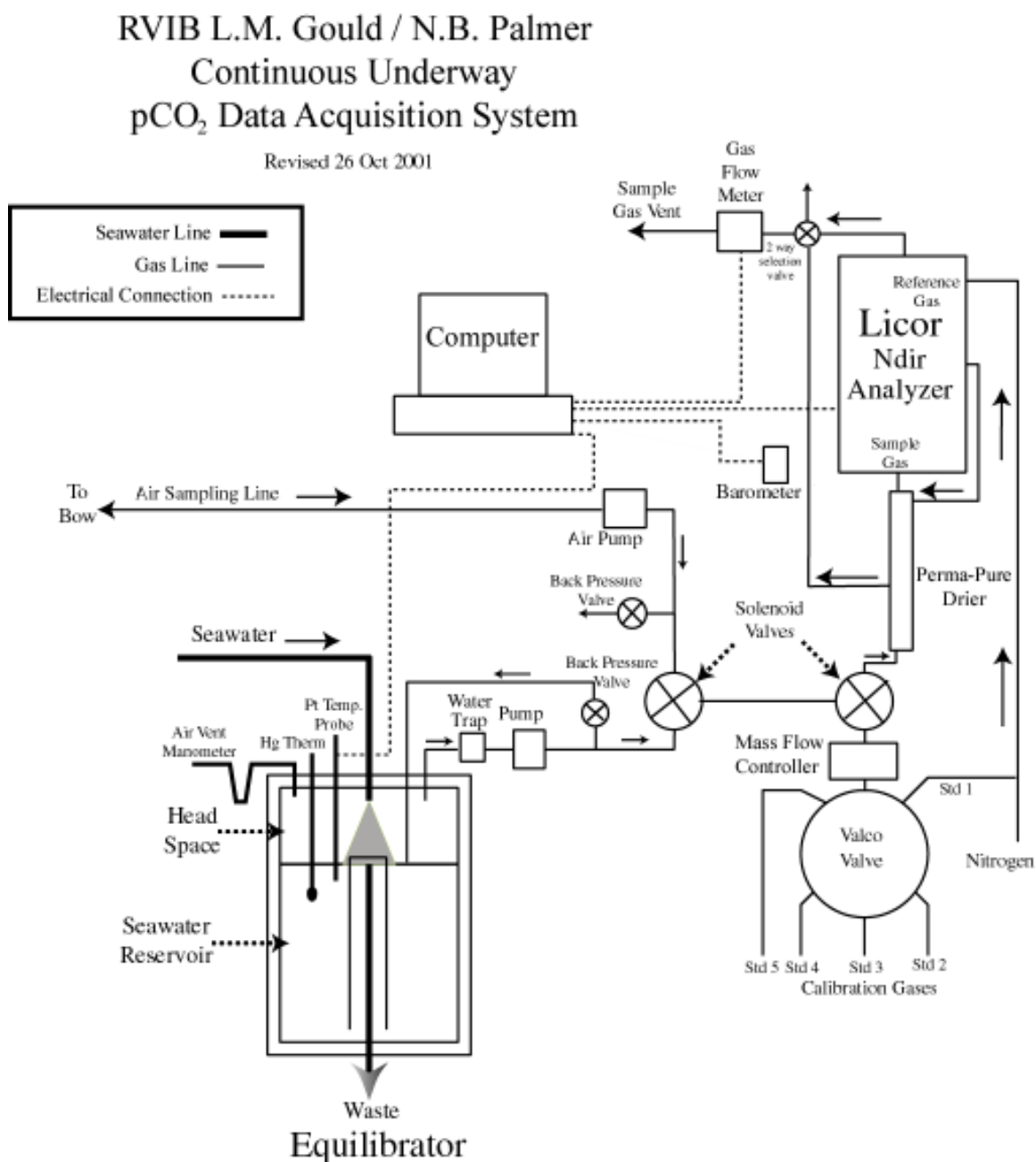
Wind speed units are meters seconds<sup>-1</sup>.

## 2. MEASUREMENTS OF $p\text{CO}_2$ IN SURFACE WATERS

### 2-a) The LDEO Underway System for Surface Water $p\text{CO}_2$ Measurements:

The system for underway measurements of  $p\text{CO}_2$  in surface waters consists of a) a water-air equilibrator, b) a non-dispersive infra-red  $\text{CO}_2$  gas analyzer and c) a data logging system. The measurement system is schematically shown in Fig. 1, and is similar with the one described in Bates et al. (1998). Each of these units and the data reduction procedures used will be described below.

Figure 1 - The underway  $p\text{CO}_2$  system used for the measurements of  $p\text{CO}_2$  in surface waters during the Southern Ocean JGOFS (AESOP) Program.



**2-b) Water-air Equilibrator:**

The equilibrator has a total volume of about 30 liters and is equipped with a

analyzer (Model 6251, Lincoln, NB) was used. After about 2 minutes of purging period, the gas flow was stopped and readings were recorded on the computer. Although an electronic circuit was provided by the manufacturer in order to linearize the CO<sub>2</sub> response, it exhibited a few inflexions that deviated from linearity by a few ppm. Therefore, we chose not to use the outputs from the linearization circuit supplied by the manufacturer. Instead, we used five standard gas mixtures (one pure nitrogen and four CO<sub>2</sub>-air mixtures) during the expeditions, and established response curves using the raw millivolt output from the analyzer. The CO<sub>2</sub> concentrations in the gas mixtures were calibrated using the SIO standards determined by C. D. Keeling's group using the manometric method. The concentrations of CO<sub>2</sub> in the standard gas mixtures were summarized above.

During normal operations, each of the standard gas mixtures was passed through the analyzer for 120 seconds at a rate of about 60 ml/min. This replaced the IR analyzer cell completely with the new gas. The flow was stopped for 10 seconds and then a millivolt reading from the analyzer was taken and recorded. Samples of equilibrated air and marine air were pumped through the analyzer for 120 seconds (2 minutes) at a rate of about 50 ml/min to purge the previous sample in the IR cell. The flow was stopped for 10 seconds and a reading for the analyzer output was recorded. This procedure was intended to eliminate errors due to fluctuations of the dynamic pressure within the IR cell by irregular gas flow rates. The slow flow rates used for samples were required for the removal of water vapor using the PermaPure membrane dryer. We analyze 20 seawater and two air samples between two sets of calibration runs using the five standard gases. (the current setup is 30 seawater samples, 5 atmospheric)

#### **2-d) Data Logging System:**

Our laptop records the following data and writes it via a serial port to the ship's RVDAS system.

Date,  
Time (GMT),  
Sample ID (standard gas cylinder numbers, seawater CO<sub>2</sub>, atmospheric CO<sub>2</sub>)  
Barometric pressure in the laboratory (to 0.1 mb)  
IR cell temperature,  
Gas flow rate in the IR cell (to 0.1 ml/min),  
Temperature of equilibration (to 0.01 °C),  
Analyzer output (millivolts to 0.1 mv)  
CO<sub>2</sub> concentration in dry gas sample (preliminary based on the last response curve), and  
pCO<sub>2</sub> (preliminary value based on the last response curve).

The ships RVDAS system adds several other data elements from various sensors and equipment. The list is:

Latitude, Longitude, Thermosalinograph temperature, thermosalinograph salinity, fluorometer voltage, wind speed, wind direction, and, barometric pressure.

**2-e) Data Reduction Procedures:**

The concentration of CO<sub>2</sub> in the sample was computed by the following way based on the millivolt reading and time of the reading. The millivolt reading taken for each of the five standard gases at the time of sample measurement was computed by linearly interpolating as a function of time using the readings taken before and after the respective standard gases were analyzed. This yields millivolt reading for each of the five standard gases at the time when the sample was analyzed. These five values were fit to a fourth-order polynomial equation (with five constants to be determined). This serves as the response curve. The CO<sub>2</sub> concentration in the sample was computed using the response curve that was established at the time of each sample analysis. This method has been demonstrated to yield more reliable CO<sub>2</sub> values compared with those computed, for example, using a least-squares fit of a quadratic or cubic functions to the five calibration points. The method described above yields atmospheric CO<sub>2</sub> values that are consistent with those reported for the South Pole and the Cape Grim by the Climate Monitoring and Diagnostics Laboratory/NOAA in Boulder, CO.

The partial pressure of CO<sub>2</sub> in seawater, (pCO<sub>2</sub>)<sub>sw</sub>, at the temperature of equilibration, T<sub>eq</sub>, in the unit of microatmospheres (μatm) was computed using the expression:

$$(pCO_2)_{sw} @ T_{eq} = (V_{CO_2})_{eq} \times (P_b - P_w), \dots \dots \dots [1]$$

(V<sub>CO<sub>2</sub></sub>)<sub>eq</sub> = the mole fraction concentration (ppm) of CO<sub>2</sub> in the dried equilibrated carrier gas;  
 P<sub>b</sub> = the barometric pressure (that is equal to the total pressure of equilibration) in atmospheres; and  
 P<sub>w</sub> = the equilibrium water vapor pressure at T<sub>eq</sub> (°C) and salinity.

The water vapor pressure was computed using the following formulation;

$$P_w \text{ (atm)} = (1/760) \times (1 - 5.368 \times 10^{-4} \times \text{Sal}) \times \text{EXP}\{[0.0031476 - (1/TK)]/1.8752 \times 10^{-4}\}, \dots \dots [2]$$

where Sal is salinity in PSU measured using the ship's thermosalinograph, and TK is the temperature of equilibration in °K.

The (pCO<sub>2</sub>)<sub>sw</sub> at the in situ temperature, T<sub>in situ</sub>, was computed using a constant value of 0.0423 % per °C for the effect of temperature (Takahashi et al., 1993):

$$(pCO_2)_{sw} @ T_{in \text{ situ}} = (pCO_2)_{sw} @ T_{eq} \times \text{EXP}[0.0423 \times (T_{in \text{ situ}} - T_{eq})].$$

The value for T<sub>in situ</sub> is taken to be the seawater temperature measured by the ship's thermosalinograph at the time of pCO<sub>2</sub> measurements. T<sub>eq</sub> is generally warmer than

Tin situ by 0.5 ~ 0.8 °C. Hence the temperature correction is normally less than 3% of pCO<sub>2</sub> values.

The over all precision of the reported pCO<sub>2</sub>sw values has been estimated to be about ±1.5 uatm.

### 3. MEASUREMENTS OF pCO<sub>2</sub> IN THE ATMOSPHERE

#### 3-a) Measurements:

The air measurement system is shown schematically in Fig. 1. Uncontaminated marine air samples were collected about 10 m above the sea surface using a DEKORON tubing (3/8 " i.d., Calco Inc., PA), a thin-wall aluminum tubing protected by plastic casing. The intake was located at the middle of the foremast about 10 m above the sea surface. A KNF Neuberger air pump that was located near the IR analyzer was used to pump air through the tubing and into the IR analyzer. Even when air samples were not directed to the analyzer, the pump was on all the time to keep the air flowing through the sampling line. For the analysis, the air sample was passed through a drying column to remove water vapor (the same PermaPure column as used for the equilibrated gas) and introduced into the IR cell for CO<sub>2</sub> analysis at a rate of about 50 ml/min. After 2 minutes of purging the cell, the flow was stopped for 10 seconds and the IR millivolt output reading was recorded.

#### 3-b) Data Processing:

The partial pressure of CO<sub>2</sub> in the air, (pCO<sub>2</sub>)air, was computed in the unit of microatmospheres (µatm) in the same way as that for seawater using Eq. [3] below:

$$(pCO_2)_{air} = (V_{CO_2})_{air} \times (P_b - P_w), \dots \dots \dots [3]$$

(V<sub>CO<sub>2</sub></sub>)<sub>air</sub> = the mole fraction concentration (ppm) of CO<sub>2</sub> in the dried air sample;  
 P<sub>b</sub> = the barometric pressure at sea surface in atmospheres; and  
 P<sub>w</sub> = the equilibrium water vapor pressure at Tin situ (°C) and salinity given by Eq. [2].

The precision of the atmospheric pCO<sub>2</sub> values have been estimated to be about ± 1 µatm.

#### **4. REFERENCES CITED**

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